Scalable Implicit Methods for Free Surface Flows in Glaciology

Scalable Ice-sheet Solvers and Infrastructure for Petascale, High-resolution, Unstructured Simulations (SISIPHUS) DOE ASCR ISICLES

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Outline

Objectives

Some opinionated commentary

Conservative steady-state energy transport

Code verification

Coupling software

High order with unassembled representations

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Antarctic Ocean-Ice Interaction



Bindschadler 2008

Glaciology and society

- Quantitative analysis of ice dynamics in changing climate
- Inversion to determine current state
- Stability and sensitivity, mostly at grounding line
- Prediect sea level rise as a function of sea surface temperature [energy policy]

Our efforts

- Unstructured meshing, geometric models of boundaries
- Fully implicit formulations to enable analysis
- Implicit solver components
 - saddle points, anisotropy, heterogeneity, transport

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- composability and multi-physics coupling
- High order accuracy and high throughput
- Adjoints using restricted AD

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Bathymetry and stickyness distribution

- Bathymetry:
 - Aspect ratio $\varepsilon = [H]/[x] \ll 1$
 - Need surface and bed slopes to be small
- Stickyness distribution:
 - Limiting cases of plug flow versus vertical shear
 - Stress ratio: $\lambda = [\tau_{xz}]/[\tau_{membrane}]$
 - Discontinuous: frozen to slippery transition at ice stream margins
- Standard approach in glaciology:

Taylor expand in ε and sometimes λ , drop higher order terms.

- $\lambda \gg 1~$ Shallow Ice Approximation (SIA), no horizontal coupling
- $\lambda \ll 1~$ Shallow Shelf Approximation (SSA), 2D elliptic solve in map-plane
 - Hydrostatic and various hybrids, 2D or 3D elliptic solves
- Bed slope is discontinuous and of order 1.
 - Taylor expansions no longer valid
 - Numerics require high resolution, subgrid parametrization, short time steps

Still get low quality results in the regions of most interest.

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Textbook multigrid efficiency



Grid-sequenced Newton-Krylov solution of test X. The solid lines denote nonlinear iterations, and the dotted lines with \times denote linear residuals.

Strong scaling on Shaheen



Strong scaling on Shaheen for different size coarse levels problems and different coarse level solvers. The straight lines on the strong scaling plot have slope -1 which is optimal.

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Conservative two-phase formulation

Find momentum density ρu , pressure p, and total energy density E:

$$(\rho u)_t + \nabla \cdot (\rho u \otimes u - \eta D u_i + p 1) - \rho g = 0$$

$$\rho_t + \nabla \cdot \rho u = 0$$

$$E_t + \nabla \cdot ((E+p)u - k_T \nabla T - k_\omega \nabla \omega) - \eta D u_i : D u_i - \rho u \cdot g = 0$$

- Solve for density ρ, ice velocity u_i, temperature T, and melt fraction ω using constitutive relations.
 - Simplified constitutive relations can be solved explicitly.
 - Temperature, moisture, and strain-rate dependent rheology η .
 - ▶ High order FEM, typically Q₃ momentum & energy, SUPG (yuck).
- DAEs solved implicitly after semidiscretizing in space.
- Newton solver converges quadratically.
- Thermocoupled steady state in one nonlinear solve
 - no time stepping needed, total cost similar to 3 semi-implicit steps
 - useful for inverse problems and stability analysis
- (Somewhat) robust preconditioning using nested field-split

Block on inclined plate, nominal Re = 0.24, Pe = 120





Contours of Energy, melt fraction up to 15%, density ratio 2.

Contours of viscous heat production, 1/r singularity at corners.

Relative effect of the blocks

$$J = \begin{pmatrix} J_{uu} & J_{up} & J_{uE} \\ J_{pu} & 0 & 0 \\ J_{Eu} & J_{Ep} & J_{EE} \end{pmatrix}.$$

- *J_{uu}* Viscous/momentum terms, nearly symmetric, variable coefficients, anisotropy from Newton.
- J_{up} Weak pressure gradient, viscosity dependence on pressure (small), gravitational contribution (pressure-induced density variation). Large, nearly balanced by gravitational forcing.
- J_{uE} Viscous dependence on energy, very nonlinear, not very large.
- J_{pu} Divergence (mass conservation), nearly equal to J_{up}^{T} .
- J_{Eu} Sensitivity of energy on momentum, mostly advective transport. Large in boundary layers with large thermal/moisture gradients.
- J_{Ep} Thermal/moisture diffusion due to pressure-melting, $u \cdot \nabla$.
- *J_{EE}* Advection-diffusion for energy, very nonlinear at small regularization. Advection-dominated except in boundary layers and stagnant ice, often balanced in vertical.

How much nesting?

$$P_{1} = \begin{pmatrix} J_{uu} & J_{up} & J_{uE} \\ 0 & B_{pp} & 0 \\ 0 & 0 & J_{EE} \end{pmatrix}$$

- *B_{pp}* is a mass matrix in the pressure space weighted by inverse of kinematic viscosity.
- Elman, Mihajlović, Wathen, JCP 2011 for non-dimensional isoviscouse Boussinesq.
- Works well for non-dimensional problems on the cube, not for realistic parameters.

$$P = \begin{bmatrix} \begin{pmatrix} J_{uu} & J_{up} \\ J_{pu} & 0 \end{pmatrix} \\ \begin{pmatrix} J_{Eu} & J_{Ep} \end{pmatrix} & J_{EE} \end{bmatrix}$$

- Inexact inner solve using upper-triangular with B_{pp} for Schur.
- Another level of nesting.
- GCR tolerant of inexact inner solves.
- Outer converges in 1 or 2 iterations.
- Low-order preconditioning full-accuracy unassembled high order operator.
- Build these on command line with PETSc PCFieldSplit.

Everything is better as a smoother

Block preconditioners work alright, but...

- nested iteration requires more dot products
- more iterations: coarse levels don't "see" each other
- finer grained kernels: lower arithmetic intensity, even more limited by memory bandwidth

Coupled multigrid

- need compatible coarsening
 - can do algebraically (Adams 2004) but would need to assemble
- stability issues for lowest order $Q_1 P_0^{\text{disc}}$
 - Rannacher-Turek looks great, but no discrete Korn's inequality
- coupled "Vanka" smoothers difficult to implement with high performance, especially for FEM
- block preconditioners as smoothers reuse software better
- one level by reducing order for the coarse space, more levels need non-nested geometric MG or go all-algebraic and pay for matrix assembly and setup







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Symbolic form of large-deformation elasticity

Find displacement vector *u* such that:

$$\int_{\Omega} \nabla v : \Pi = 0, \quad \forall v$$

where

$$F = I - \nabla u$$

$$E = (F^{T}F - I)/2$$

$$S = \lambda (tr E)I + 2\mu E$$

$$\Pi = F \cdot S$$

Deformation gradient Green-Lagrange tensor Second Piola-Kirchoff tensor First Piola-Kirchoff tensor

- # Identity tensor
- # Deformation gradient
- # Green-Lagrange tensor
- # Second Piola-Kirchoff tensor
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Deformation gradient Green-Lagrange tensor Second Piola-Kirchoff tensor $S = \lambda (J^2 - I)C^{-1} + \mu (I - C^{-1})$ Neo-Hookean material, $(C = F^T F)$

Identity tensor # Deformation gradient # Green-Lagrange tensor # Second Piola-Kirchoff tensor # First Piola-Kirchoff tensor

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Manufactured solution

 Apply strong-form nonlinear differential operator symbolically to define

$$f(x, y, z) = \nabla \cdot \Pi(\nabla u_{\mathsf{exact}})$$

Solve finite element problem for u_h

$$\int_{\Omega} \nabla v : \Pi(\nabla u_h) = \int v \cdot f(x, y, z), \quad \forall v$$

• Compute norms of $u_h - u_{\text{exact}}$.

Manufactured solution



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Convergence rates

			$\ u_h - u\ _2$		$\ u_h - u\ _{\infty}$		$\ \nabla u_h - \nabla u\ _2$		$\ \nabla u_h - \nabla u\ _{\infty}$	
Mesh		# Nodes	Error	Ø	Error	Ø	Error	Ø	Error	\mathscr{O}
Q_1	13	8	1.79e+00	_	6.50e-01	_	3.70e+00	_	1.08e+00	_
Q_1	2^{3}	27	5.49e-01	1.71	3.40e-01	0.93	1.61e+00	1.20	6.92e-01	0.64
Q_1	4 ³	125	1.53e-01	1.84	1.26e-01	1.43	8.01e-01	1.01	4.51e-01	0.62
Q_1	8 ³	729	3.94e-02	1.96	3.73e-02	1.76	3.98e-01	1.01	2.81e-01	0.68
Q_1	16^{3}	4913	9.95e-03	1.99	1.01e-02	1.88	1.98e-01	1.01	1.57e-01	0.84
Q_1	32 ³	35937	2.49e-03	2.00	2.61e-03	1.95	9.92e-02	1.00	8.32e-02	0.92
Q_3	13	64	4.14e-02	_	2.71e-02	_	2.90e-01	_	1.63e-01	_
Q_3	2^{3}	343	2.06e-03	4.33	2.06e-03	3.72	2.39e-02	3.60	1.14e-02	3.84
Q_3	4 ³	2197	1.81e-04	3.51	2.06e-04	3.32	4.23e-03	2.50	2.88e-03	1.98
Q_3	8 ³	15625	1.22e-05	3.89	1.87e-05	3.46	5.79e-04	2.87	5.84e-04	2.30
Q_5	1 ³	216	3.76e-03	_	2.90e-03	_	4.69e-02	_	3.16e-02	_
Q_5	2^{3}	1331	7.58e-05	5.63	5.92e-05	5.61	1.62e-03	4.86	1.05e-03	4.91
Q_5	4 ³	9261	7.33e-07	6.69	6.61e-07	6.48	2.59e-05	5.97	1.76e-05	5.90
Q_9	13	1000	5.81e-05	_	5.04e-05	_	1.42e-03	_	1.05e-03	_
Q_9	2^{3}	6859	6.27e-08	9.86	7.59e-08	9.38	1.63e-06	9.77	1.60e-06	9.36

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ALE form

After discretization in time ($\alpha \propto 1/\Delta t$) we have a Jacobian

$$\begin{bmatrix} A_{II} & A_{I\Gamma} & & & \\ \alpha M_{\Gamma\Gamma} & -N_{\Gamma\Gamma} & & \\ G_{II} & G_{\Gamma I} & B_{II} & B_{I\Gamma} & C_I^T & D_I \\ G_{I\Gamma} & G_{\Gamma\Gamma} & B_{\Gamma I} & B_{\Gamma\Gamma} & C_{\Gamma}^T & D_{\Gamma} \\ G_{Ip} & G_{\Gamma p} & C_I & C_{\Gamma} & & \\ \alpha E_I & \alpha E_{\Gamma} & F_I & F_{\Gamma} & \alpha M_{\Theta} + J \end{bmatrix} \begin{bmatrix} x_I \\ x_{\Gamma} \\ u_I \\ u_{\Gamma} \\ p \\ \Theta \end{bmatrix}$$

mesh motion equations (Laplace-Beltrami or pseudo-elasticity)

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- $(\dot{x} u) \cdot n =$ accumulution
- "just" geometry
- Stokes problem
- temperature dependence of rheology
- convective terms and strain heating in heat transport
- thermal advection-diffusion



- package each "physics" independently
- solve single-physics and coupled problems
- semi-implicit and fully implicit
- reuse residual and Jacobian evaluation unmodified
- direct solvers, fieldsplit inside multigrid, multigrid inside fieldsplit without recompilation
- use the best possible matrix format for each physics (e.g. symmetric block size 3)

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- matrix-free anywhere
- multiple levels of nesting

MomentumStokes Pressure

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Boundary Layer

Ocean

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Performance of assembled versus unassembled



- Same linear operator, smaller to not store unassembled
- Use local symbolic math or AD, runtime choice of order, precondition with low-order method
- Dual order h and p FEM: github.com/jedbrown/dohp

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PETSc: mcs.anl.gov/petsc

Automation

- ► For unassembled representations, decomposition, and assembly
- Continuous weak form: find u

$$v^T F(u) \sim \int_{\Omega} v \cdot f_0(u, \nabla u) + \nabla v \cdot f_1(u, \nabla u) = 0, \quad \forall v \in \mathscr{V}_0$$

▶ Weak form of the Jacobian *J*(*w*): find *u*

$$v^{T}J(w)u \sim \int_{\Omega} \begin{bmatrix} v^{T} & \nabla v^{T} \end{bmatrix} \begin{bmatrix} f_{0,0} & f_{0,1} \\ f_{1,0} & f_{1,1} \end{bmatrix} \begin{bmatrix} u \\ \nabla u \end{bmatrix}$$
$$[f_{i,j}] = \begin{bmatrix} \frac{\partial f_{0}}{\partial u} & \frac{\partial f_{0}}{\partial \nabla u} \\ \frac{\partial f_{1}}{\partial u} & \frac{\partial f_{1}}{\partial \nabla u} \end{bmatrix} (w, \nabla w)$$

- Terms in $[f_{i,j}]$ easy to compute symbolically, AD more scalable.
- ► Nonlinear terms *f*₀,*f*₁ usually have the most expensive nonlinearities in the computation of scalars
 - Equations of state, effective viscosity
 - Compute gradient with reverse-mode, store at quadrature points.
 - Perturb scalars, then use forward-mode to complete the Jacobian.

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Flip forward/reverse for action of the adjoint.

Outlook

- Stabilized continuous FEM is terrible, need to implement DG for transport.
- Issues defining conservative normals for slip: all-positive (e.g. spline) basis?
- Geometric coupling to surface causes delicate stiffness at large time steps.
- Visualization should have hooks for solving equations of state.
- Need good hierarchical solver diagnostic tools.
- Solution transfer after remeshing.
- Have active set and semi-smooth Newton for contact, but there are many types of contact and much work to be done.
- Strongly Coupled Solvers with Loosely Coupled Software CP76 11:00 tomorrow, Room 304.